



Reliability of rock-fall protection galleries

A case study with a special focus on the uncertainty modeling

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Overview



- Introduction
- Probabilistic modeling of rock detachment frequencies
- Modeling the rock-fall process
- Resistance of rock-fall protection galleries
- Conclusion

Introduction



- The increase of the traffic in mountainous regions necessitate protection structures against natural hazards.
- Difficult or impossible to describe loads due to such hazards in codified format.
- These events are rare, site specific and object related.
- Due to the lack of a codified format, inconsistent decisions are made in regard to the reliability of protection structures.
- Only a risk-based approach can ensure optimal the choice and design of a protection structure.

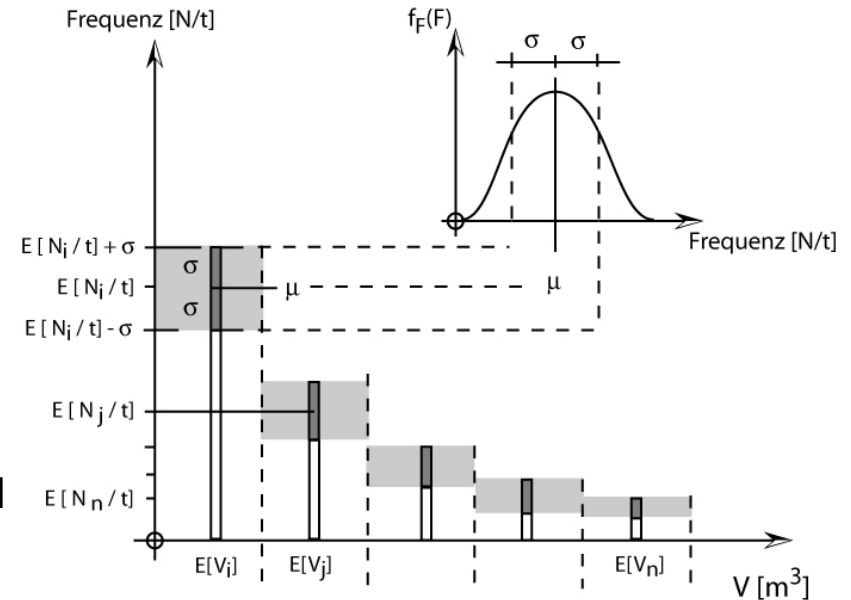
Introduction



- A case study has been carried out on an existing rock-fall gallery built in 1975 in the Swiss alps.
- A geological expertise for the special case was analyzed.
- The steepness slope was modified for this study to obtain higher energies.
- All diagrams and graphs which are shown in this presentation are results of this case study.

Probabilistic modeling of the rock-fall frequency

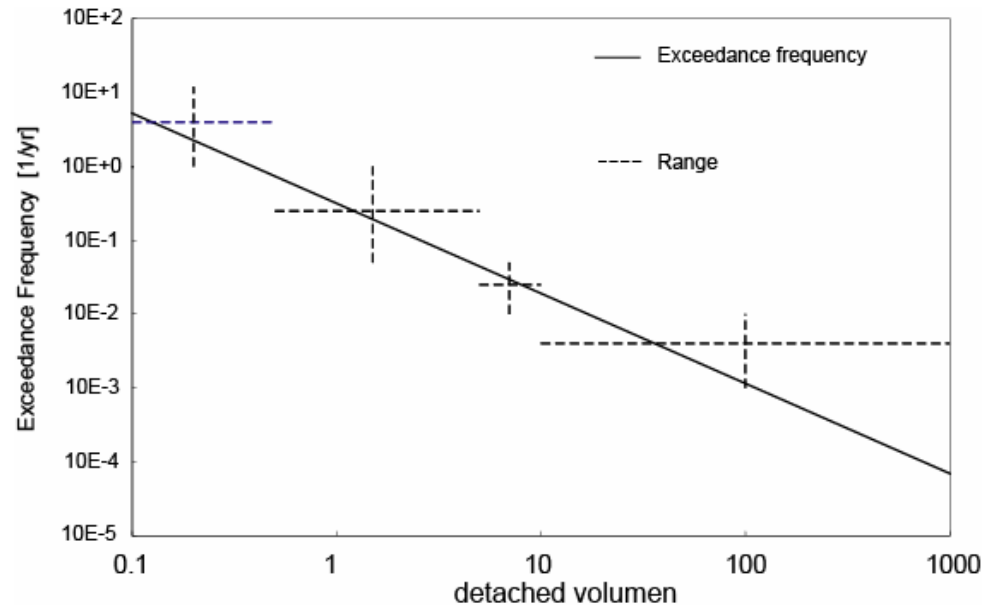
- Due to the highly specific nature of rock-fall, no or only few quantitative data is available.
- Geological expertises are traditionally of a qualitative or semi-quantitative character.
- For a probabilistic approach it is necessary to model these information and the inherent uncertainties.



Probabilistic modeling of the rock-fall frequency

- Most exceptional loads are described by their exceedance frequency
- In the present study case a power-law is applied – without any physical or mathematical foundation.
- The exceedance frequency of a detached rock is defined as

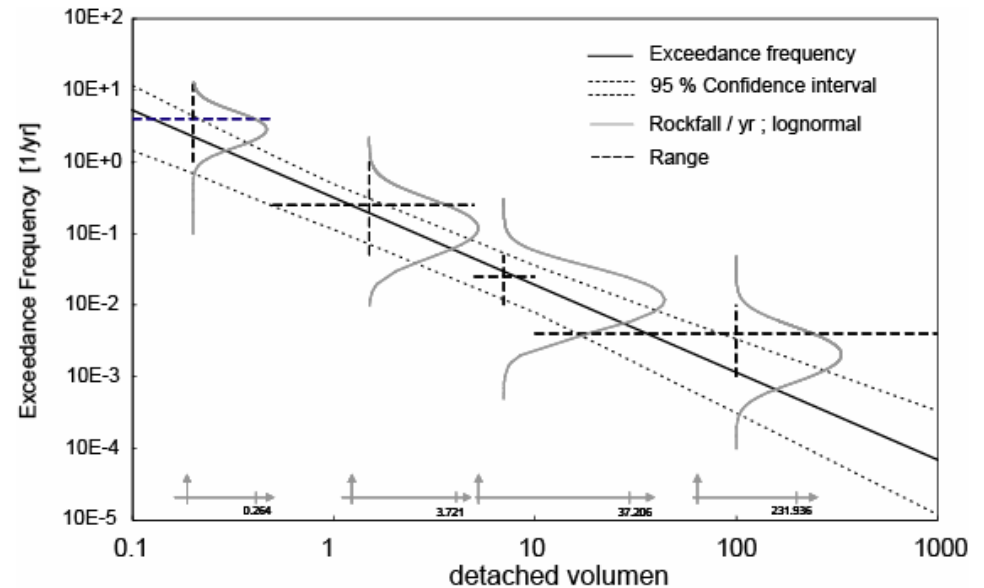
$$H_V(v | a, b) = a \cdot v^{-b}$$



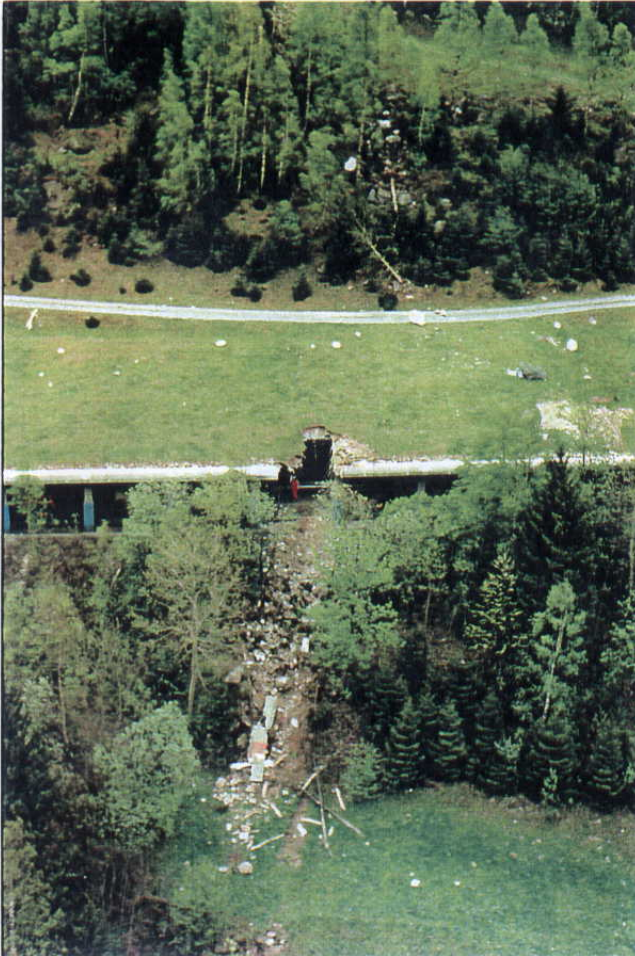
Probabilistic modeling of the rock-fall frequency

- The uncertainty in this estimation can be quantified by fitting a probability density function to the estimated frequency.
- From the geological expertise, distributions are then fitted for each given volume range.
- The parameters a and b are then estimated together with the uncertainty on the estimation.
- The predictive frequency distribution of a detachment is calculated by:

$$h_V(v) = \int_{-\infty}^{\infty} \int_{-\infty}^{\infty} h_V(v | a, b) \cdot f_{a,b}(a, b) da db$$



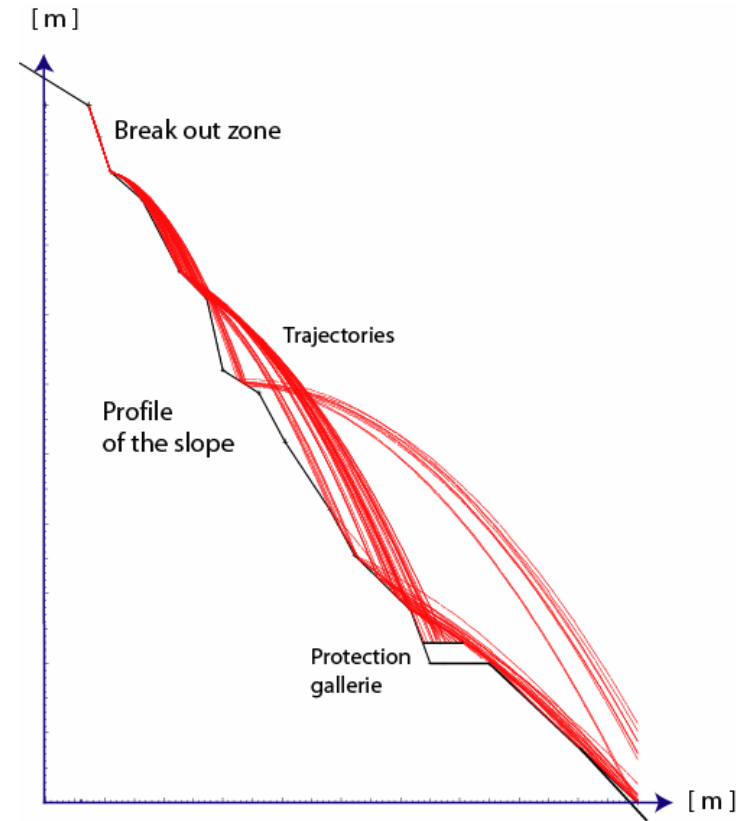
Modeling the rock-fall Process



- Once a stone is detached the falling process determines the kinetic energy of the stone.
- The main parameters describing the falling process are
 - Profile of the slope
 - Coefficient of restitution
 - geology
 - morphology
 - vegetation
 - structure of the contact surface

Modeling the rock-fall Process

- The falling process is simulated by standard rock-fall programs.
- They are based on a Monte Carlo simulation.
- Using these programs, parameter studies can be performed.
- Simulations over the possible range of rock-volumes.



Modeling the rock-fall Process

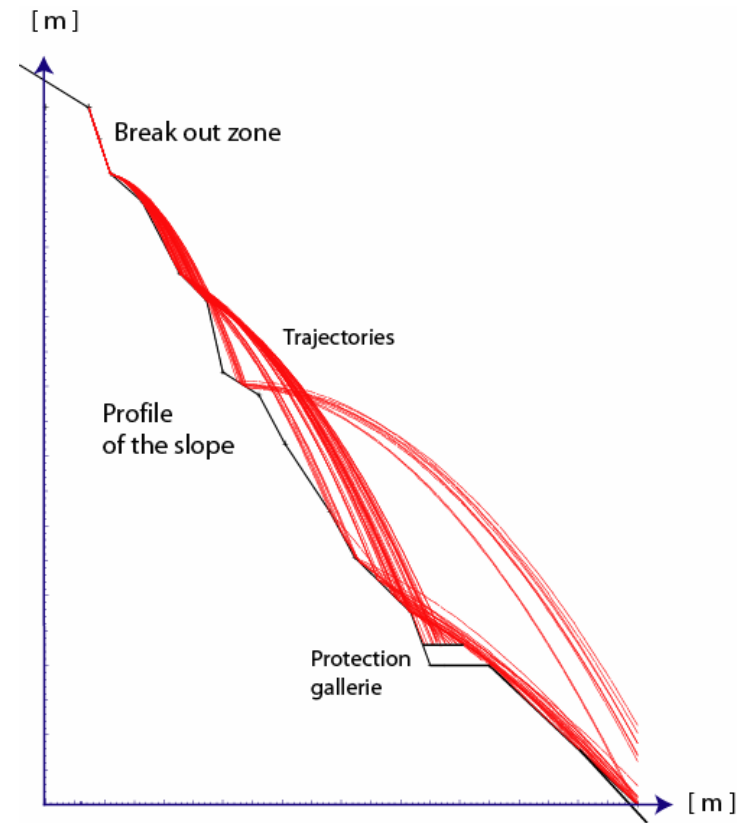
- With these simulations a PDF of the energy at the gallery conditional on the detached volume is obtained.

$$f_E^G(e|v)$$

- The joint frequency distribution of volumes and energies of the rocks hitting the gallery can then be calculated :

$$h_{EV}^G(e, v) = f_E^G(e|v) \cdot h_V(v)$$

$$H_{EV}^G(e, v) = \int_e^\infty \int_v^\infty f_E^G(e/v) h_V(v) dv de$$

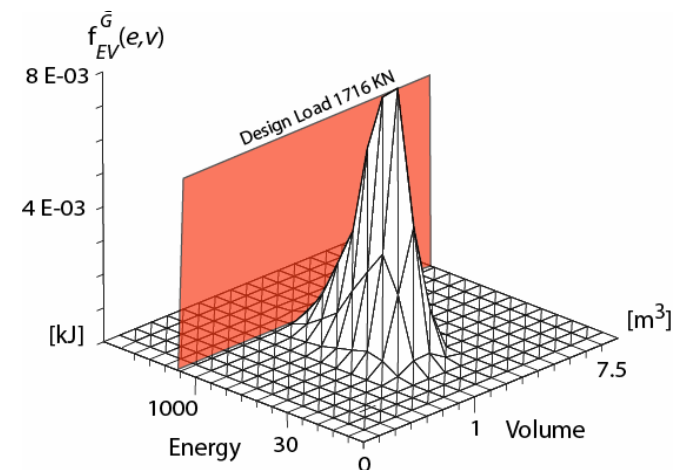
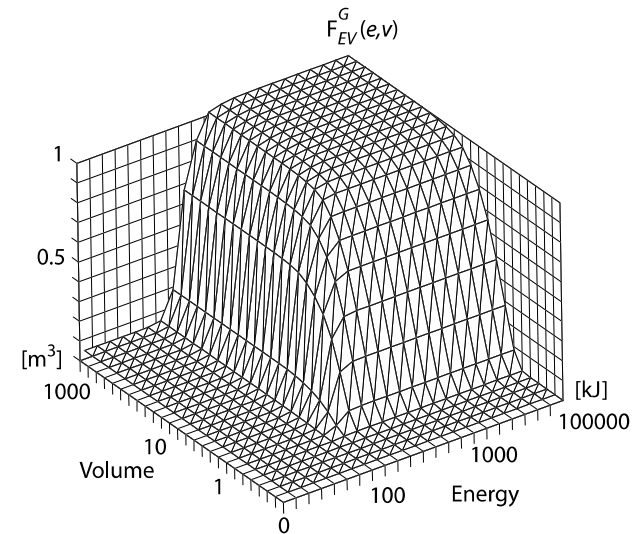


Modeling the rock-fall Process

- For the calculation of the reliability of rock-fall protection structures the extreme value is of interest.
- Assuming rock-fall follows a Poisson process, the CDF is:

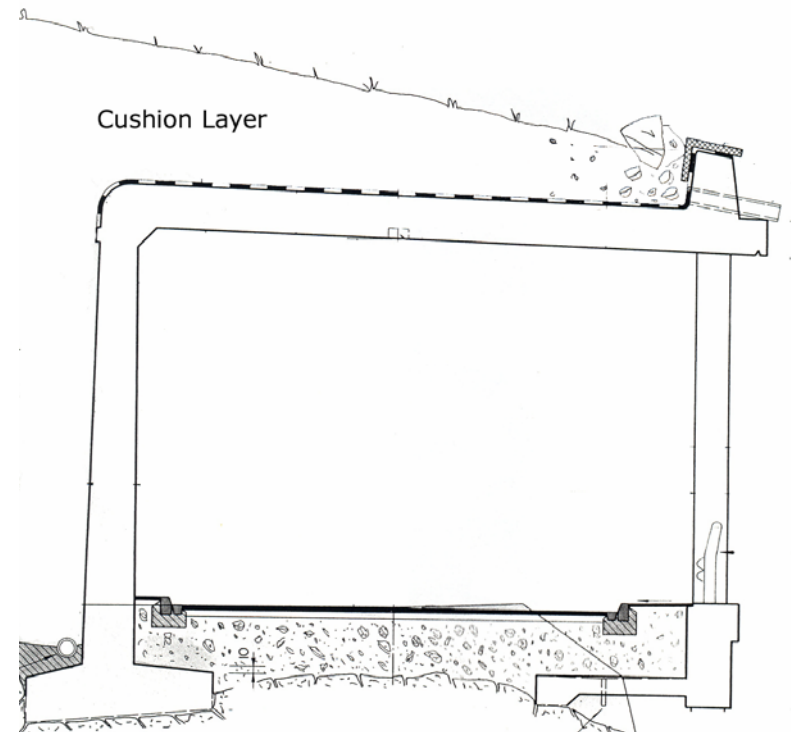
$$F_{EV}^G(e, v) = 1 - e^{-H_{EV}^G(e, v)}$$

- The original design load was 1716 KN
~ 300 yr.
- This estimation is conservative for this gallery.



Resistance

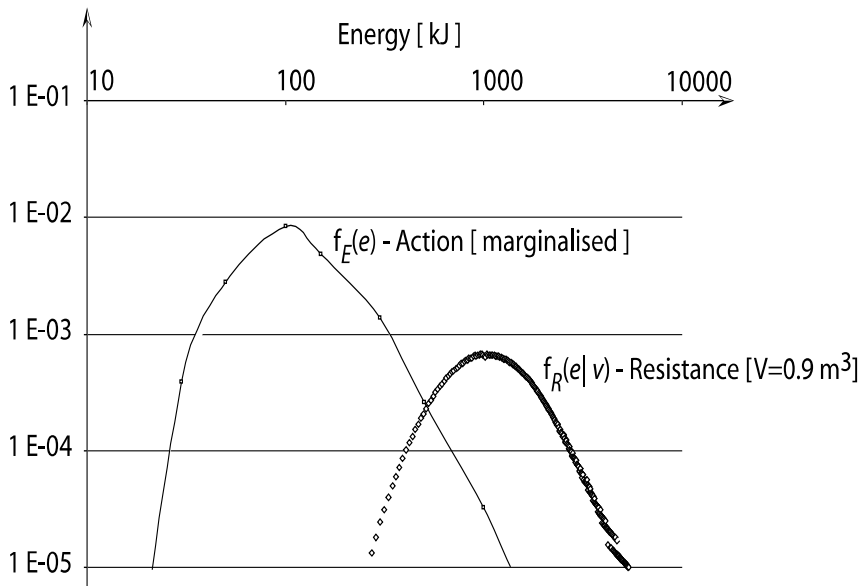
- On most of the protection galleries a cushion layer is present.
- This layer mitigates the so called "hard impact".
- It dissipates the energy of the rocks and share it to a larger area
- In our studies a static equivalent load for the dynamic impact is assumed.





Resistance

- The main failure mechanism is punching.
- With a model for the resistance against punching shear it is possible to perform a reliability analysis.



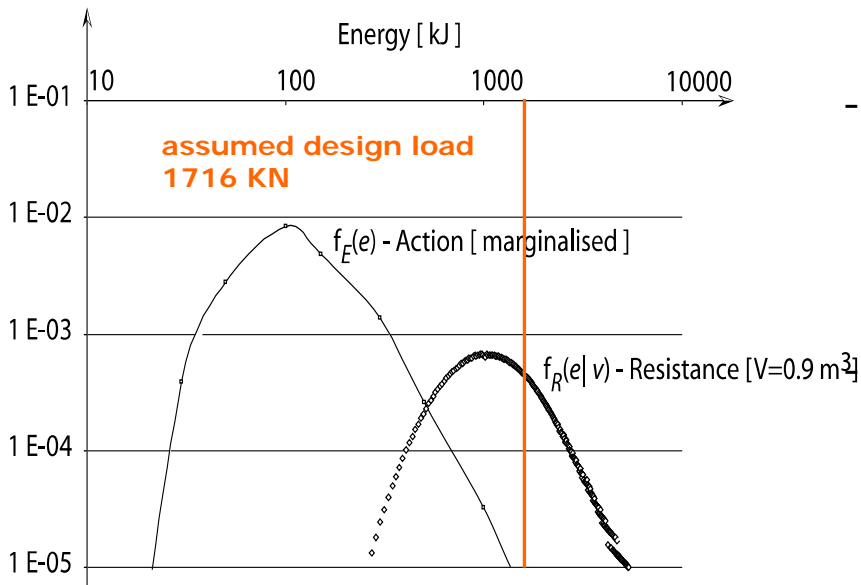


Probability of failure

- With the assumed steepness of the slope the probability of failure for the gallery was calculated:

$$P_f = \int_{-\infty}^{\infty} F_R(EV) \cdot f_S(EV) dV dE$$

$$P_f = 6.34 \text{ E} - 03 \text{ [yr}^{-1} \text{]} = 1/158 \text{ yr}$$



- There was no failure at this location until now

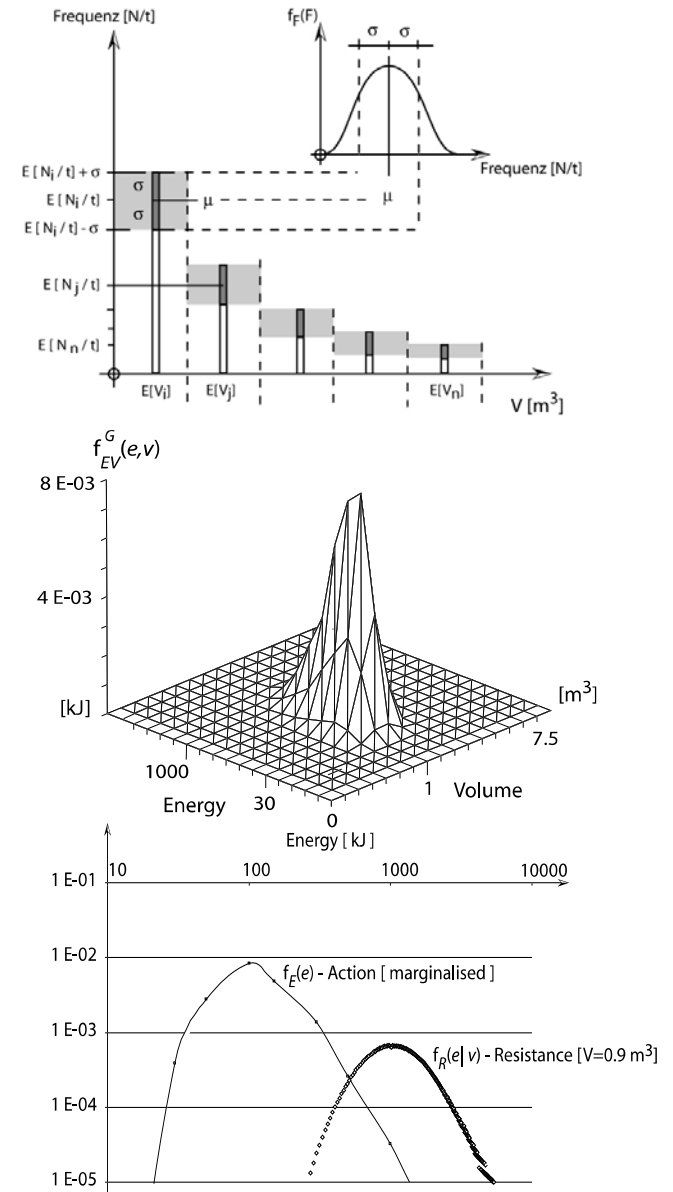
- The slope is not steep enough to reach such energy

The resistance of the gallery is undervalued in regard to the design load

- In the early 70th punching was not considered

Conclusions

- This approach enables to deal with semi-quantitative statements and assess a predictive frequency distribution of rock fall events.
- A model for reliability analysis of rock-fall protection galleries has been developed.
- It is possible to derive and verify design loads for new and existing structures
- This facilitates the optimal planning of risk mitigation actions





Reliability of rock-fall protection galleries

Thank you for your attention

