

Risk and Safety in Engineering

Loads and Resistance

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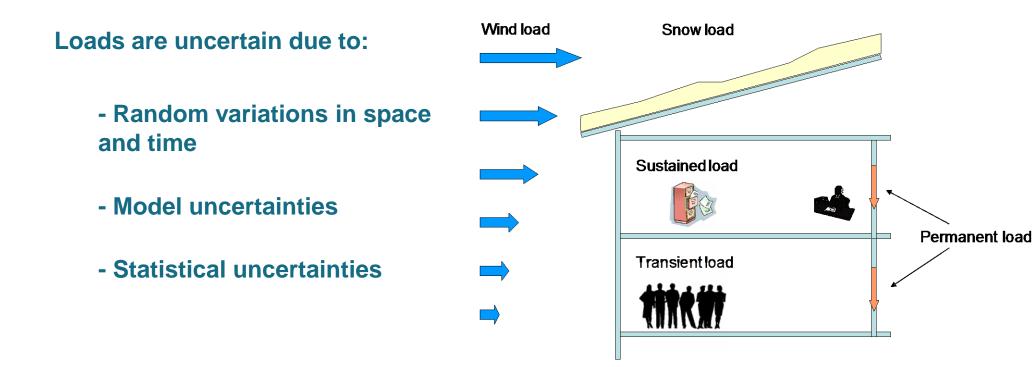
• Time Variability

• Probabilistic Modelling of Resistances

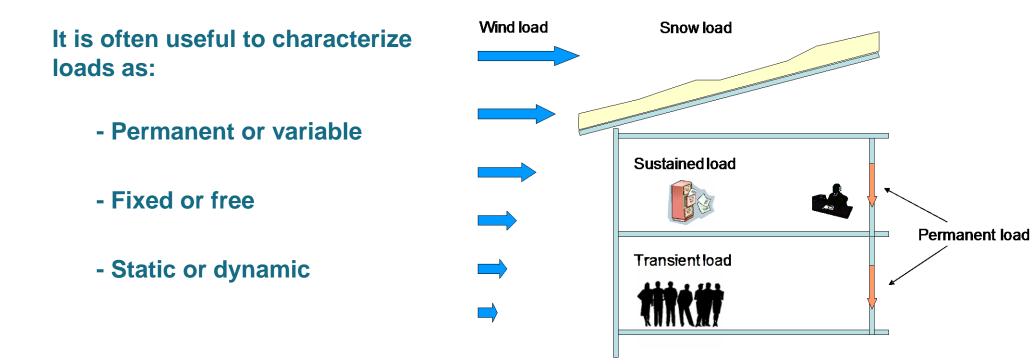
• Probabilistic Modelling of Model Uncertainties

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Loads on Structures



Loads on Structures



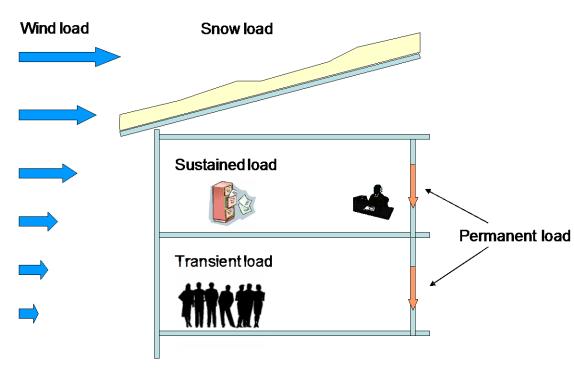
Loads on Structures

The probabilistic modelling includes the following steps:

- specifying the definition of the random variables used to represent the uncertainties in the loading

- selecting a suitable distribution type to represent the random variable

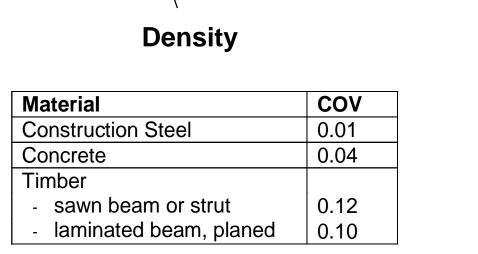
- assigning the distribution parameters of the selected distribution.

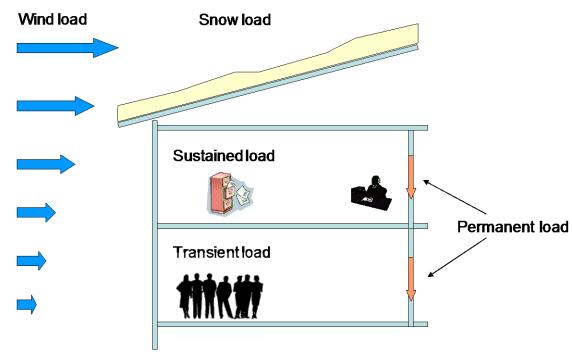


Loads on Structures

Permanent loads:

 $G = \int_{V} \gamma dV$





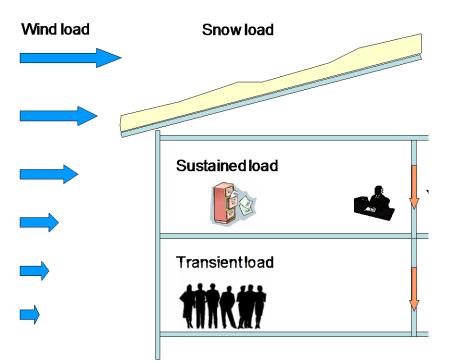
Loads on Structures

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Live floor loads:
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$$W(x, y) = m + V + U(x, y)$$

m is the overall mean value for a given use category

- V is a zero mean random variable
- *U*(*x*,*y*) is a zero mean random field



Loads on Structures

Wind loads

$$w = c_a c_g c_r \overline{Q}_{ref} = c_a c_e \overline{Q}_{ref}$$

$$w = c_d c_a c_e \overline{Q}_{ref}$$

$$Q = \frac{1}{2}\rho U^2$$

Q_{ref} : 10 min mean U

Smaller rigid structures

Taller flexible structures

 c_r : roughness factor c_g : gust factor c_a : aero-dynamic shape factor c_d : dynamic factor c_e : exposure factor ρ : 1.25 kg/m³

Loads on Structures

Wind loads

 c_r : roughness factor c_g : gust factor c_a : aero-dynamic shape factor c_d : dynamic factor c_e : exposure factor ρ : 1.25 kg/m³

Variable	Туре	V
Q_{ref}	Gumbel	0.20 - 0.30
C _r	Lognormal	0.10 - 0.20
c_a - coefficient pressure	Lognormal	0.10 - 0.30
coefficient force	Lognormal	0.10 - 0.15
C _g	Lognormal	0.10 - 0.15
C _d	Lognormal	0.10 - 0.20

Wind load can be assumed to be Log-Normal distributed

$$V_w^2 \cong V_{c_d}^2 + V_{c_a}^2 + V_{c_r}^2 + V_{\overline{Q}_{ref}}^2$$

 $V_w^2 \cong V_{c_a}^2 + V_{c_r}^2 + V_{\overline{Q}_{ext}}^2$

Dynamic sensitive

Rigid

Loads on Structures

Snow loads

$$S_r = S_g r k^{\frac{h}{h_r}}$$

$$S_g = d \cdot \rho(d)$$

 S_r : Snow load on roof S_g : Snow load on ground r: ground to roof conversion factor k: location factor (1.25 coastal, 1,5 inland) h: altitude in meters h_r : reference altitude (300 meters) ρ : 1.25 kg/m³

Typically the snow load is modelled by a Gamma or a Gumbel distribution

Stochastic Processes

Random variables represent random events, e.g. properties of objects

If we look at random events over time we speak about random processes to represent these.

Very often we speak implicitly about random processes in structural engineering

Examples:

- Earthquake with a return period of 475 years
- 100 yearly flood
- Maximum loads during the lifecycle of a structure

Stochastische Prozesse

 In many engineering problems we need to be able to describe the random variations in time more specifically:

The occurrences of events at random discrete points in time (rock-fall, earthquakes, accidents, queues, failures, etc.)

- Poisson process, exponential and Gamma distribution

The random values of events occurring continuously in time (wind pressures, wave loads, temperatures, etc.)

- Continuous random processes (Normal process)

Discrete event of flood



Continuous stress variations due to waves



- A sequence of experiments with two possible exclusive outcomes is called Bernoulli Trial.
- The outcomes are typically called success and failure.

Example:

Cars in a street; leave road: failure, probability *p*

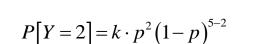
straight: success, probability 1- p

Probability that two of five cars leave the road?

Probability that none(of 5) leaves: $P[Y=0]=(1-p)(1-p)...(1-p)=(1-p)^{5}$

Probability that two (of 5) leave:

Binomialdistribution:



 $p_{Y}(y) = \binom{n}{v} p^{y} (1-p)^{n-y}$

k = number of possibilities 2 of 5

- A sequence of experiments with two possible exclusive outcomes is called Bernoulli Trial.
- The outcomes are typically called success and failure.

Example:

Cars in a street; leave road: failure, probability p

straight: success, probability 1- p

Probability that two of five cars leave the road? $P[Y=0] = (1-p)(1-p)...(1-p) = (1-p)^{5}$

Probability that none(of 5) leaves:

Probability that two (of 5) lea

Binomialdistribution:

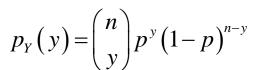
leave:
$$P[Y=2] = k \cdot p^2 (1-p)^{5-2}$$

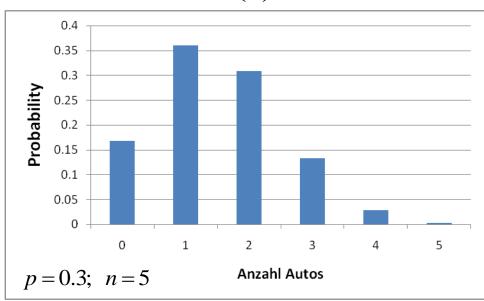
 $p_Y(y) = {n \choose y} p^y (1-p)^{n-y}$
 $p_Y(2) = {5 \choose 2} 0.3^2 (1-0.3)^{5-2} = 0.3087$

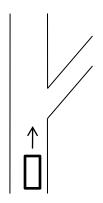
• Example:

Cars in a street; leave road: failure, probability p = 0.3

• Binomialdistribution:





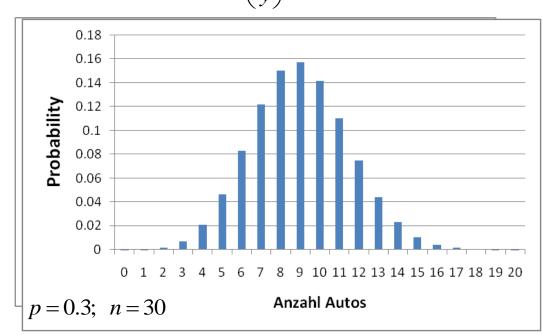


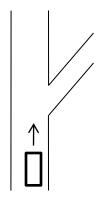
• Example:

Cars in a street; leave road: failure, probability p = 0.3

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- Binomialdistribution:

$$p_{Y}(y) = \binom{n}{y} p^{y} (1-p)^{n-y}$$





E[Y] = np

Var[Y] = np(1-p)

In practice the number of trials is often not possible to estimate (very large or unknown)

$$n \to \infty \quad p \to 0 \quad np = u \to const. \qquad p = u / n$$
$$p_{Y}(y) = {n \choose y} (v/n)^{y} (1 - (v/n))^{n-y} \xrightarrow{\text{im Limit}}_{n \to \infty} \rightarrow \frac{u^{y} e^{-u}}{y!}$$
$$p_{X}(x) = \frac{u^{x} e^{-u}}{x!} \qquad \text{Poissondistribution}$$

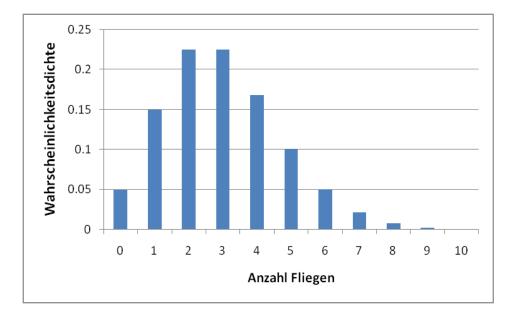
Poissondistrbution:

$$p_X(x) = \frac{u^x e^{-u}}{x!}$$

Moments:

E[X] = u Var[X] = u

Frequency *u* = 3 per Minute.



What about the number of events in 10 Minutes: 3 per Minute -> 30 per 10 Minutes

u can be skaled over time:

u = vt

Poissondistribution:

$$p_{X}(x) = \frac{u^{x}e^{-u}}{x!} = \frac{(vt)^{x}e^{-vt}}{x!}$$

The sequence of events that might be described with a Poisson Distribution is called Poisson Process.

$$E[X] = u = vt$$
$$Var[X] = u = vt$$

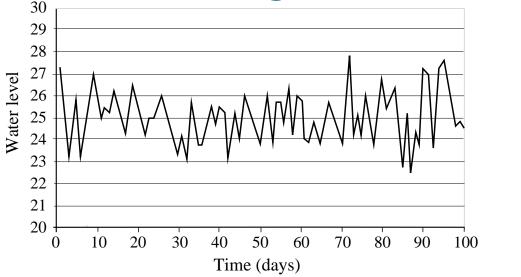
 The Poisson counting process is one of the most commonly applied families of probability distributions applied in reliability theory

Requirements:

- 1) the probability of one event in the interval $(t,t+\Delta t)$ is asymptotically proportional to Δt .
- 2) the probability of more than one event in the interval $(t,t+\Delta t)$ is 0 for $\Delta t \rightarrow 0$.
- 3) events in disjoint intervals are mutually independent.

Continuous random processes

A continuous random process is a random process which has realizations continuously over time and for which the realizations belong to a continuous sample space.



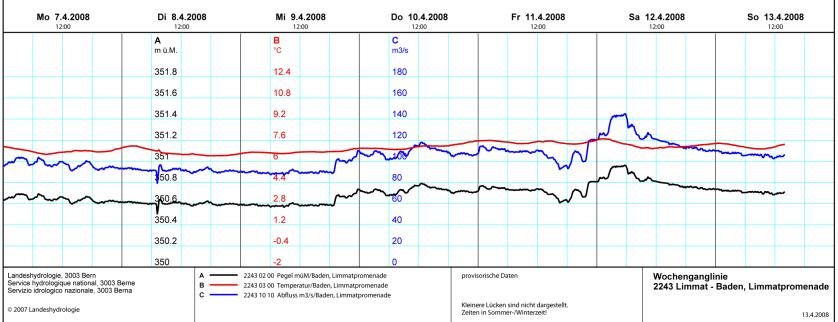
Variations of; water levels wind speed rain fall

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- •
- •

Realization of continuous scalar valued random process

Realisation of a continuous process

- Water level.



Continuous random processes

The mean value of the possible realizations of a random process is given as:

$$\mu_X(t) = E[X(t)] = \int_{-\infty}^{\infty} x f_X(x;t) dx$$

Function of time !

The correlation between realizations at any two points in time is given as:

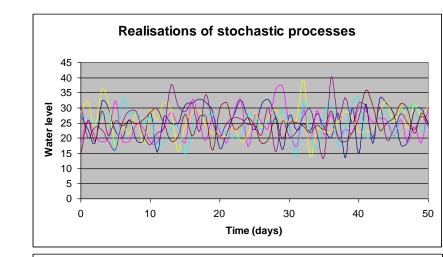
$$R_{XX}(t_1, t_2) = E[X(t_1)X(t_2)] = \int_{-\infty}^{\infty} \int_{-\infty}^{\infty} x_1 x_2 f_{XX}(x_1, x_2; t_1, t_2) dx_1 dx_2$$

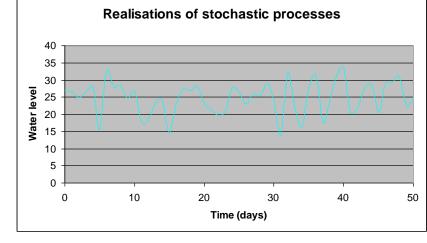
Auto-correlation function – refers to a scalar valued random process

Properties

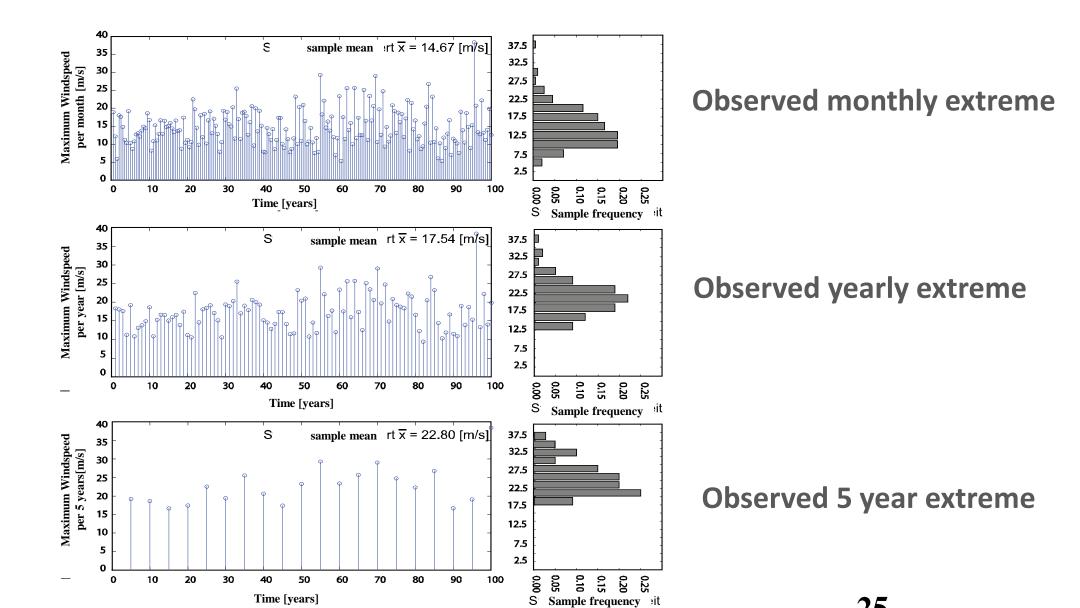
A random process is said to be *strictly stationary* if all its moments are invariant to a shift in time.

A random process is said to be strictly ergodic if it is strictly stationary and in addition all its moments may be determined on the basis of one realization of the process.

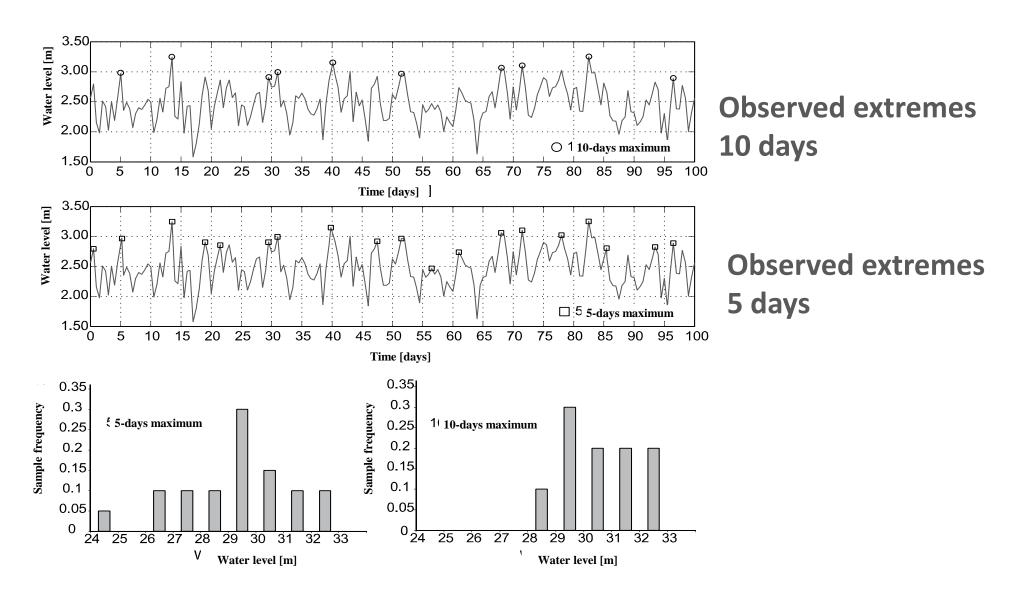




Time dependency – e.g. Windspeed:



Time dependency – e.g. Water level:



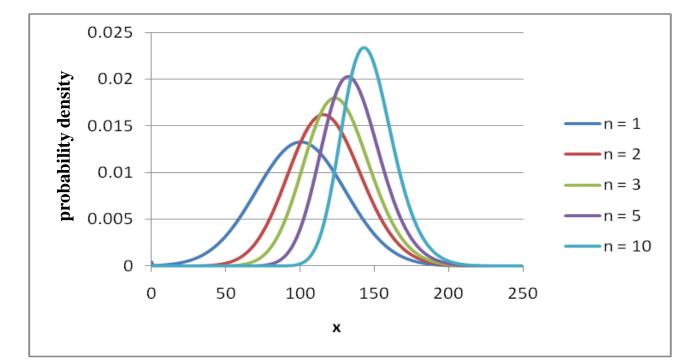
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Time dependency – Extreme value distributions:

Assuming the extreme values within a period *T* of an ergodic random process X(t) are independent and follow the probability distribution $F_{X,T}^{\max}(x)$ Then, the extreme values of the same process within the period

 $n \cdot T$

Are following:



$$F_{X,nT}^{\max}(x) = \left(F_{X,T}^{\max}(x)\right)^n$$

Extreme Value Distributions

Extreme Type I – Gumbel Max

When the upper tail of the probability density function falls off exponentially (exponential, Normal and Gamma distribution) then the maximum in the time interval *T* is said to be Type I extreme distributed

$$f_{X,T}^{\max}(x) = \alpha \exp(-\alpha(x-u) - \exp(-\alpha(x-u)))$$

$$F_{X,T}^{\max}(x) = \exp(-\exp(-\alpha(x-u)))$$

$$\mu_{X_T^{\max}} = u + \frac{\gamma}{\alpha} = u + \frac{0.577216}{\alpha}$$

 $\sigma_{X_T^{\max}} = \frac{\pi}{\alpha\sqrt{6}}$

For increasing time intervals the variance is constant but the mean value increases as: $\mu_{X_{nT}^{\max}} = \mu_{X_{T}^{\max}} + \frac{\sqrt{6}}{\pi} \sigma_{X_{T}^{\max}} \ln(n)$

Extreme Value Distributions

Extreme Type II – Frechet Max

When a probability density function is downwards limited at zero and upwards falls off in the form

$$F_X(x) = 1 - \beta (\frac{1}{x})^k$$

then the maximum in the time interval *T* is said to be Type II extreme distributed

$$F_{X,T}^{\max}(x) = \exp\left(-\left(\frac{u}{x}\right)^{\kappa}\right)$$

$$f_{X,T}^{\max}(x) = \frac{k}{u} \left(\frac{u}{x}\right)^{k+1} \exp\left(-\left(\frac{u}{x}\right)^{k}\right)$$

Mean value and standard deviation
$\mu_{X_T^{\max}} = u\Gamma(1 - \frac{1}{k})$
$\sigma_{X_T^{\max}}^2 = u^2 \left[\Gamma(1 - \frac{2}{k}) - \Gamma^2(1 - \frac{1}{k}) \right]$

Extreme Value Distributions

Extreme Type III – Weibull Min

When a probability density function is downwards limited at ε and the lower tail falls off towards ε in the form $F(x) = c(x - \varepsilon)^k$

then the minimum in the time interval *T* is said to be Type III extreme distributed

$$F_{X,T}^{\min}(x) = 1 - \exp\left(-\left(\frac{x-\varepsilon}{u-\varepsilon}\right)^{k}\right)$$
$$f_{X,T}^{\min}(x) = \frac{k}{u-\varepsilon} \left(\frac{x-\varepsilon}{u-\varepsilon}\right)^{k-1} \exp\left(-\left(\frac{x-\varepsilon}{u-\varepsilon}\right)^{k}\right)$$

Mean value and standard deviation $\mu_{X_T^{\min}} = \varepsilon + (u - \varepsilon)\Gamma(1 + \frac{1}{k})$ $\sigma_{X_T^{\min}}^2 = (u - \varepsilon)^2 \left[\Gamma(1 + \frac{2}{k}) - \Gamma^2(1 + \frac{1}{k})\right]$

Return Period

The return period for extreme events T_R may be defined as:

$$T_R = n \cdot T = \frac{1}{\left(1 - F_{X,T}^{\max}\left(x\right)\right)}$$

Example:

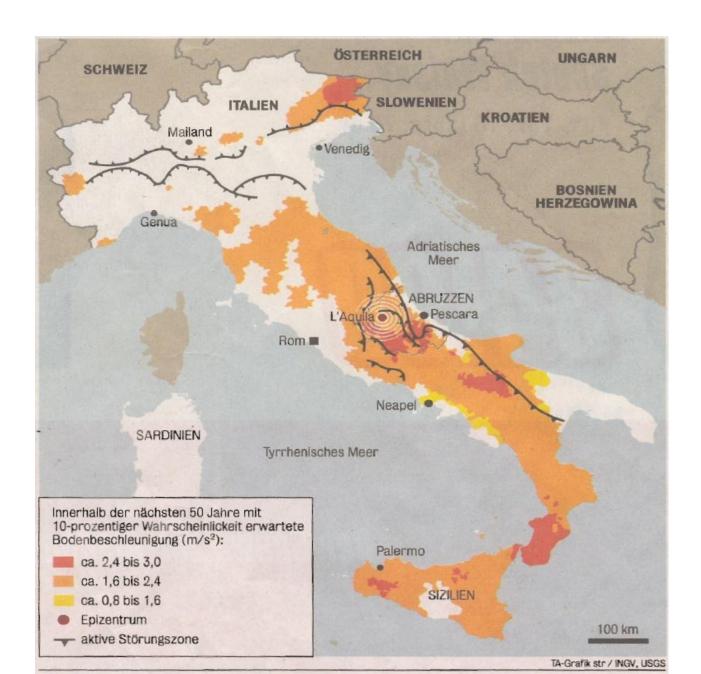
Let us assume that - according to the cumulative distribution function of the annual maximum traffic load the annual probability that a truck load larger than 100 ton is equal to 0.02 – then the return period of such heavy truck events is:

$$T_R = n \cdot T = \frac{1}{0.02} \Longrightarrow n = \frac{1}{1 \cdot 0.02} = 50$$
 years

Example

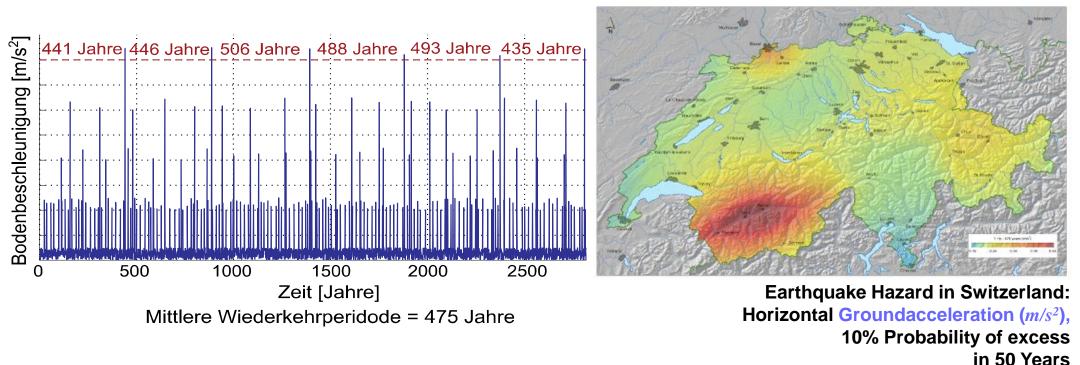
A Earthquake hazard map represents the ground acceleration in (m/s^2) with a return period of 475 years.

Tages-Anzeiger Tuesday, 07. April 2009



Exercise

A Earthquake hazard map represents the ground acceleration in (m/s^2) with a return period of 475 years.



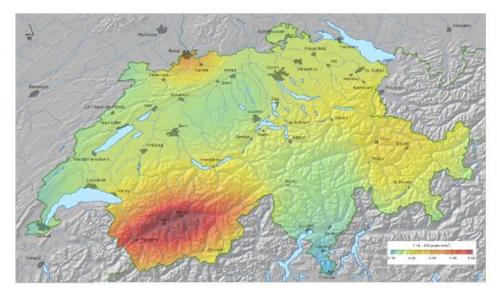
www.earthquake.ethz.ch

Excercise

A Earthquake hazard map represents the ground acceleration in (m/s^2) with a return period of 475 years.

- a) Show that Return period 475 Years is equal to 10% Probability of excess in 50 Years
- b) How large is the probability that an earthquake with that return period happens within 475 years?

Homogenious Poisson Process



Earthquake Hazard in Switzerland: Horizontal Groundacceleration (m/s²), 10% Probability of excess in 50 Years www.earthquake.ethz.ch

Solution

a) Show that Return period 475 Years is equal to 10% Probability of excess in 50 Years

yearly occurrence probability:

$$p = \frac{1}{T} = \frac{1}{475}$$

mean time between two successive events:

$$E[T] = \frac{1}{p} = \frac{1}{\frac{1}{475}} = 475$$

The time between two successive events for Poisson processes is exponential distributed.

$$E[T] = \frac{1}{\nu} = 475$$
 $\nu = \frac{1}{E[T]} = \frac{1}{475}$

$$P[T \le 50 Jahre] = 1 - e^{-\nu(t) \cdot t} = 1 - e^{-\frac{1}{475} \cdot 50} = 0.1$$

Solution

b) How large is the probability that an earthquake with that return period happens within 475 years?

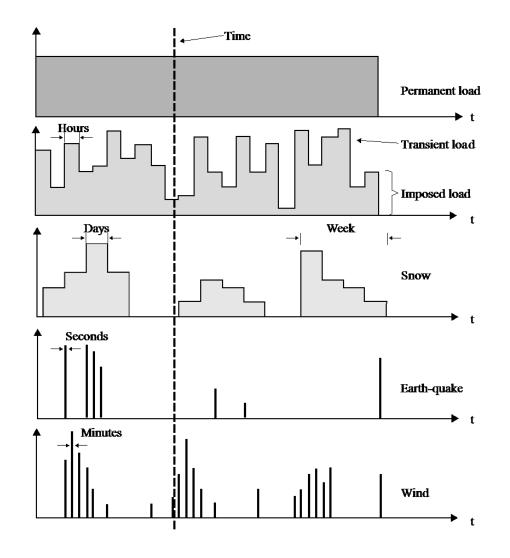
$$P[T \le 475] = 1 - e^{-\nu(t) \cdot t} = 1 - e^{-\frac{1}{475}475} = 1 - \frac{1}{e} = 0.63$$

Loads on Structures

Combination of loads

We are interested in the maximum of a sum of load effects from different loads

$$X_{max}(T) = \max_{T} \{ X_{1}(t) + X_{2}(t) + \dots + X_{n}(t) \}$$



Loads on Structures

Combination of loads

Turkstra's load combination rule

We take the max of the following combinations

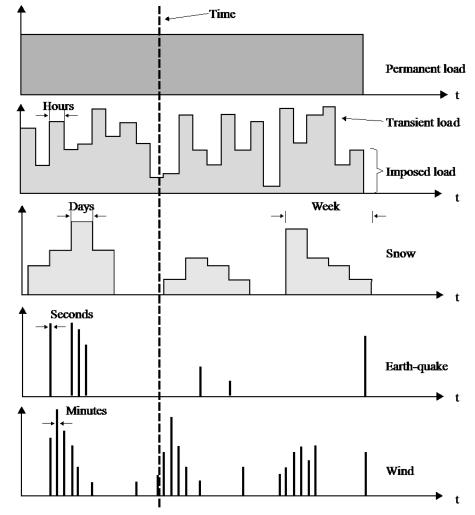
$$Z_{1} = \max_{T} \{X_{1}(t)\} + X_{2}(t^{*}) + X_{3}(t^{*}) + \dots + X_{n}(t^{*})$$

$$Z_{2} = X_{1}(t^{*}) + \max_{T} \{X_{2}(t)\} + X_{3}(t^{*}) + \dots + X_{n}(t^{*})$$

$$\vdots$$

$$Z_{n} = X_{1}(t^{*}) + X_{2}(t^{*}) + X_{3}(t^{*}) + \dots + \max_{T} \{X_{n}(t)\}$$

$$X_{max}(T) \approx \max_{i} \{Z_{i}\}$$



Uncertainties of resistances

In structural engineering resistances include the following uncertainties

- Geometrical uncertainties
- Material characteristics
- Model uncertainties

Random variation in time and space

The steps in the modelling process are:

- define the random variables used to represent the uncertainties in the resistances
- select a suitable distribution type to represent the random variable
- to assign the distribution parameters of the selected distribution.

Uncertainties of resistances

Concrete compressive strength

$$f_c = \alpha(t, \tau) f_{co}^{\lambda}$$

 f_{co} :28 day compressive strength $\alpha(t, \tau)$:spatial stress and loading time function λ :conversion factor between in-situ concretestrength and cylinder compressive strength

The concrete compressive strength can be assumed to be Log-Normal distributed with a coefficient of variation equal to 15%

Uncertainties of resistances

Reinforcement steel yield strength

 $f_s = X_1 + X_2 + X_3$

- X_1 normal distributed random variable representing the variation in the mean of different mills.
- X_2 normal distributed zero mean random variable, which takes into account the variation between batches
- X_3 normal distributed zero mean random variable, which takes into account the variation within a batch.

Uncertainties of resistances

Reinforcement steel yield strength

Variable	Туре	E[X]	$\sigma_x[MPa]$	V_x
X_1	Normal	μ	19	-
X_2	Normal	0	22	-
<i>X</i> ₃	Normal	0	8	-
А	-	A _{nom}	-	0.02

 μ : nominal steel grade + two standard deviations of X_1

Yield stress depends on diameter of reinforcement bars

 $\mu(d) = \mu(0.87 + 0.13 \exp(-0.08d))^{-1}$

Uncertainties of resistances

Structural steel yield strength

Description	Variable	Туре	E[X]	V_X
Yield stress	f_y	Lognormal	$f_{y sp} \alpha e^{-uV_{fy}} - C$	0.07
ultimate stress	f_u	Lognormal	$B E[f_u]$	0.04
modulus of elasticity	Ε	Lognormal	E _{sp}	0.03
Poisson's ratio	V	Lognormal	V _{sp}	0.03
ultimate strain	E _u	Lognormal	$\mathcal{E}_{u \ sp}$	0.06

	f_y	f_u	Ε	V	E _u
f_y	1	0.75	0	0	-0.45
f_u		1	0	0	-0.60
E			1	0	0
v	Syn	nmetry		1	0
E _u					1

Distribution characteristics

Dependencies

Model uncertainties

Model uncertainties relate engineering model results with actual structural behaviour

$$X = \Xi \cdot X_{mod}$$
X:true value Ξ :model uncertainty X_{mod} :model value $\xi = \frac{x_{mod}}{x_{exp}}$ x_{exp} :experimentally obtained value

The JCSS Probabilistic Model Code (PMC)
 <u>http://www.jcss.ethz.ch/publications/publications_pmc.html</u>

Part I : Basis of design Part II: Load models Part III: Resistance models Part IV: Examples

• The JCSS PMC – Load Models

2.00	GENERAL PRINCIPLES	05.2001
2.01	SELF WEIGHT	06.2001
2.02	LIVE LOAD	05.2001
2.06	LOAD IN CAR PARKS	05.2001
2.12	SNOW LOAD	05.2001
2.13	WIND LOAD	05.2001
2.15	WAVE LOAD	05.2006
2.17	EARTHQUAKE	09.2002
2.18	IMPACT LOAD	05.2001
2.20	<u>FIRE</u>	05.2001

• The JCSS PMC – Resistance models

3.00	GENERAL PRINCIPLES	03.2001
3.01	CONCRETE	05.2002
3.02	STRUCTURAL STEEL	03.2001
3.0*	REINFORCING STEEL	03.2001
3.04	PRESTRESSING STEEL	04.2005
3.05	TIMBER	05.2006
3.07	SOIL PROPERTIES	06.2002
3.07 3.09	SOIL PROPERTIES MODELUNCERTAINTIES	06.2002 03.2001