

Method of Finite Elements II:

Examples 6.14 and 6.15.

Natalie Germann

**Prof. M. H. Faber, Chair of Risk and Safety,
Institute of Structural Engineering, ETH Zurich.**

Non-linear analysis

Table 1 Classification of non-linear analysis in solid and structural mechanics (taken from Bathe [1996]).

Type of analysis	Description	Typical formulation used	Stress and strain measures
Materially-nonlinear-only	Infinitesimal displacements and strains; the stress-strain relation is nonlinear	Materially-nonlinear-only (MNO)	Engineering stress and strain
Large displacements, large rotations, but small strains	Displacements and rotations of fibers are large, but fiber extensions and angle changes between fibers are small; the stress-strain relation may be linear or nonlinear	Total Lagrangian (TL) Updated Lagrangian (UL)	Second Piola-Kirchhoff stress, Green-Lagrange strain Cauchy stress, Almansi strain
Large displacements, large rotations, and large strains	Fiber extensions and angle changes between fibers are large, fiber displacements and rotations may also be large; the stress-strain relation may be linear or nonlinear	Total Lagrangian (TL) Updated Lagrangian (UL)	Second Piola-Kirchhoff stress, Green-Lagrange strain Cauchy stress, logarithmic strain

Kinematic description

1. Total Lagrangian (TL) formulation:

$$\int_{^0V} {}^{t+\Delta t}_0 S_{ij} \delta {}^{t+\Delta t}_0 e_{ij} d^0V = {}^{t+\Delta t}R. \quad (1)$$

2. Updated Lagrangian (UL) formulation:

$$\int_{^tV} {}^{t+\Delta t}_t S_{ij} \delta {}^{t+\Delta t}_t e_{ij} d^tV = {}^{t+\Delta t}R. \quad (2)$$

Kinematic variables

1. Stress measures:

- Cauchy stress tensor ${}^t\boldsymbol{\tau}$
- Second Piola-Kirchhoff stress tensor:

$${}^t_0\mathbf{S} = \frac{{}^0\rho}{{}^t\rho} {}^0_0\mathbf{X} {}^t\boldsymbol{\tau} {}^0_0\mathbf{X}^T. \quad (3)$$

2. Strain measures:

- Almansi strain tensor:

$${}^t_0\mathbf{A} = \frac{1}{2} \left(\mathbf{1} - ({}^t_0\mathbf{X} {}^t_0\mathbf{X}^T)^{-1} \right). \quad (4)$$

- Green-Lagrange strain tensor:

$${}^t_0\mathbf{E} = \frac{1}{2} ({}^t_0\mathbf{X}^T {}^t_0\mathbf{X} - \mathbf{1}). \quad (5)$$

Example 6.14

Show: Components of second Piola-Kirchhoff stress tensor are invariant under rigid body rotation of material.

Example 6.15

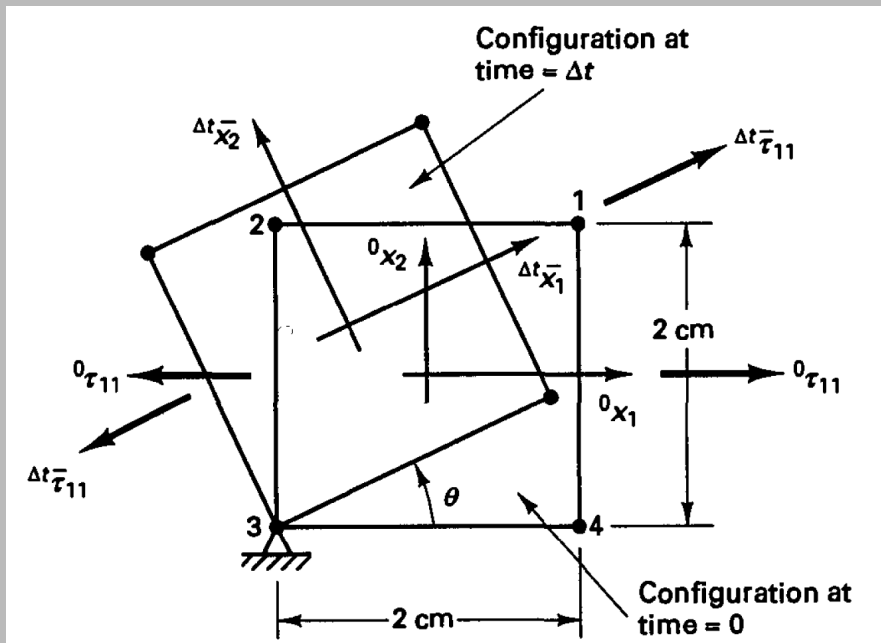


Fig. 1 Four-node element with initial stress subjected to rotation (from Bathe [1996]).

Given: Four-node element with initial stress τ_{11} at time $t = 0$ is subjected to rigid body rotation from time $t = 0$ to time $t = \Delta t$ through angle θ .

Show: Components of second Piola-Kirchhoff stress tensor did not change as a result of rigid body rotation.